

## An Introduction to Global Atmospheric Modelling

### Lecture 4: Numerical Formulation in CCMs

#### Content:

- Numerical Formulation in Atmospheric Chemistry Models
- Methods to Solve Differential Equations
- Steps in Model Formulation

#### Outline

Lecture 4: Numerical Formulation, page 2

- Lecture 1 (27 April): Introduction to Global Atmospheric Modelling
- Lecture 2 (04 May): Physical Climate Models & Fundamentals Atmospheric Radiation
- Lecture 3 (11 May): Fundamentals: Chemistry
- Lecture 4 (18 May): Numerical Formulation in CCMs & Steps in Model Formulation
- Lecture 5 (25 May): Introduction into NCAR Command Language (NCL)
- Lecture 6 (1 June): NCL practice (Dr Mattia Righi) **Doppelstunde**

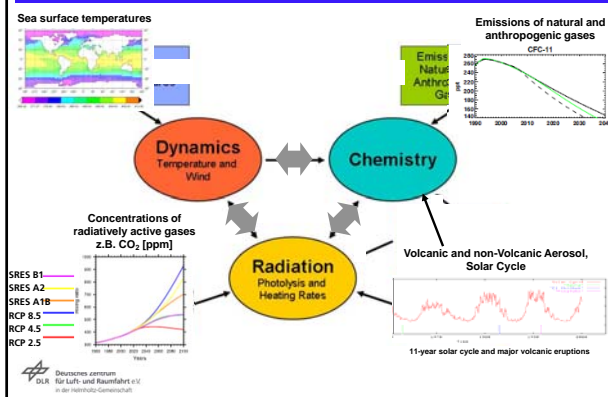
#### Preliminary schedule:

- Lecture 7 (8 June): moved to 1 June
- Lecture 8 (15 June): Fundamentals: Dynamics
- Lecture 9 (22 June): Model Evaluation and uncertainties in climate projections
- Lecture 10 (29 June): International climate modelling activities: Part 1
- Lecture 11 (6 July): EXAM
- Lecture 12 (13 July): International climate modelling activities: Part 2
- Lecture 13 (20 July): Summary

**Final Exam:** 6 July 2012, 8:00-10:00

#### Gekoppelte Chemie-Klima Modelle (CCMs)

Lecture 4: Numerical Formulation, page 3



## Numerical Formulation

#### Building a chemical model

Lecture 4: Numerical Formulation, page 5

$$\frac{d[y_i]}{dt} = P_i - L_i[y_i]$$

P: Chemical Production

L: Chemical Loss

#### Equation for Chemical Box Models

Lecture 4: Numerical Formulation, page 6

Determination of  $C_i$  (Determination of chemical loss and production rates)

$$C_i = \frac{d[y_i]}{dt} = P_i - L_i[y_i]$$

$$P_i = \sum_{j \neq i} k_{ji}[j][I] + \sum_{m \neq i} j_m[m]$$

$$L_i = \sum_j k_{ij}[j] + k_i$$

$k_{ji}$ : reaction coefficients  
 $j_m$ : photolysis rates

#### Different chemical reactions

- bi-molecular
- tri-molecular
- thermal decay
- heterogeneous
- photolysis

Determination of  $C_i$  implies simultaneous solution of up to hundreds of coupled differential equations, containing many non-linear reactions.

Reaction Rate Coefficients Lecture 4: Numerical Formulation, page 7

**How do we determine the reaction rate coefficients?**

↓

**Chemical Kinetics**

The study of reaction rates (the change in reactant and product concentrations as a function of time).

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Factors that Effect Reaction Rates Lecture 4: Numerical Formulation, page 8

**A. Concentration** – As concentration increases, the reaction rate increases.  
**Reaction Rate  $\propto$  Concentration**

**B. Physical State of Reactants** – Reactants must mix and collide in order to react.

**C. Temperature** – As temperature increases, the reaction rate increases.  
**Reaction Rate  $\propto$  Temperature**

**D. Catalyst** – A substance that increases the rate of a reaction without being consumed in the process.

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The Differential Rate Law Lecture 4: Numerical Formulation, page 9

How does the rate of the reaction depend on concentration? E.g.

$3A + 2B \rightarrow C + D$   
 $\text{rate} = k [A]^m [B]^n$

$\swarrow$   $\uparrow$   $\uparrow$   
 (Specific reaction)  $m+n$ :  $m$ :  $n$ :  
 rate constant  $\text{Order of reaction with respect to A}$   $\text{Order of reaction with respect to B}$   $\text{Overall order of the reaction}$

Each reaction is characterized by its own rate constant, depending on the nature of the reactants and the temperature  
 In general, the order with respect to each reagent must be found experimentally (not necessarily equal to stoichiometric coefficient)

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Elementary Processes and Rate Laws Lecture 4: Numerical Formulation, page 10

Reaction mechanism:  
 The collection of elementary processes by which an overall reaction occurs  
 The order of an elementary process is predictable

Unimolecular	$A^* \rightarrow B$	$k [A]$	First order
Bimolecular	$A + B \rightarrow C + D$	$k [A] [B]$	Second order
Termolecular	$A + B + C \rightarrow D + E$	$k [A] [B] [C]$	Third order

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Chemical Kinetics Lecture 4: Numerical Formulation, page 11

A reaction

**$A + B \rightarrow \text{products}$**

proceeds at a rate proportional to the concentrations raised to some power

$$\text{Rate} = \frac{d[A]}{dt} = \frac{d[B]}{dt} = k [A]^a [B]^b$$

- $k$  is the rate coefficient (rate constant). The powers  $a$  and  $b$  are the order of the reaction with respect to the reactants i.e.  
 $\alpha A + \beta B \rightarrow \text{products}$
- If for example  $a=b=1$  then the reaction is called a second order reaction ( $\alpha+\beta=2$ ).

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Chemical Kinetics: Bimolecular Reactions Lecture 4: Numerical Formulation, page 12

A reaction

**$A + B \rightarrow C + D$**

proceeds at a rate proportional to the concentrations raised to some power

$$\frac{d[A]}{dt} = -\frac{d[C]}{dt} = -k_b [A] [B]$$

- $k$  is the rate coefficient (rate constant).
- $k_b$  can be calculated by Arrhenius Law: the rate of a chemical reaction increases exponentially with the absolute temperature.

$$k_b = A e^{-\frac{E_a}{RT}}$$

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**B. Arrhenius Equation**

- Summarizes the tenets of collision theory into an equation that can be used to calculate the rate constant for a reaction.

$$k = \text{rate constant} = A e^{-E_a/RT}$$

Frequency factor      Fraction of molecules with sufficient energy

$$R = 8.315 \times 10^{-3} \text{ kJ/K}\cdot\text{mol}$$

$T$  = temperature (K)

**B. Arrhenius Equation**

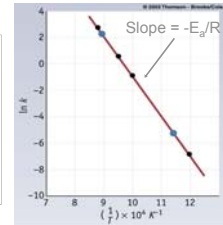
- $E_a$  can be determined by finding  $k$  for a reaction experimentally at several temperatures.

$$k = A e^{-E_a/RT}$$

Take  $\ln$  and rearrange

$$\ln(k) = \ln\left(A e^{-E_a/RT}\right) \Rightarrow \ln k = -\frac{E_a}{R} \left(\frac{1}{T}\right) + \ln A$$

$y = \quad \quad \quad mx + b$



A reaction



proceeds at a rate proportional to the concentrations raised to some power

$$\frac{d[A]}{dt} = -k_t[A][B]$$

$$k_t(M, T) = \frac{k_0(T)[M]}{1 + (k_0(T)[M]/k_\infty(T))} \cdot F(M, k_0(T), k_\infty(T))$$

High pressure case

$$k_\infty = \lim_{[M] \rightarrow \infty} k_t(M, T)$$

Low pressure case

$$k_0 = \lim_{[M] \rightarrow 0} k_t(M, T)$$

Fit between low and high pressure case

$$\log_{10} F \cong \frac{\log_{10} F_c}{1 + [\log_{10}(k_0(T)[M])/k_\infty(T)]^2}$$

Determination of  $k_0$  and  $k_\infty$  in the lab at  $T=300\text{K}$

$$k_{0-1}(T) = k_{0-1}^{300}(T/300)^{-m(0)}$$

JPL catalogue:  $k_0, n, k_\infty, m$

A reaction



Reactions that occur at the interface between condensed and gaseous phases, i.e. the surface

In liquids, the reactions tend to be inside the particle.

In solids, the diffusion from the surface is extremely small, and the reactions are confined to the surface.

$$\frac{d[A]}{dt} = -k_{het}[A][B]$$

On liquid surfaces

$$k_{het} = \frac{\omega A \gamma}{4}$$

$$\omega = \sqrt{8k_B T / \pi m}$$

A: surface

$\gamma$ : uptake coefficient

On solid surfaces

$$k_{het,s} = \frac{\gamma \pi^2 \omega [A] n}{1 + 3\gamma_s r / (4l_a)}$$

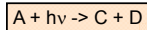
[A]: concentration

$l_a$ : mean free path length

$r$ : radius

$\gamma$ : sticking coefficient (reaction probability)

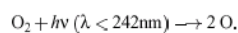
First order reaction



Time Dependence for A ( $J$  is the photolysis frequency [ $\text{s}^{-1}$ ]):

$$\frac{d[A]}{dt} = -J[A]$$

Example:



Species A undergoes photodissociation.

Reaction  $i$ :  $A + h\nu \rightarrow \text{products}$

$$\left. \frac{d[A]}{dt} \right|_{\text{reac } i} = -[A] \cdot \underbrace{\int \sigma_X(\lambda) \phi_i(\lambda, T, \dots) E(\lambda, \dots) d\lambda}_{\text{Reaction rate coefficient } j}$$

A concentration rate of change due to photolysis reaction  $i$

Reaction rate coefficient  $j$

$$J = \int_{\lambda} \sigma(\lambda) \Phi(\lambda) \int_{\omega} I(\lambda, \theta, \phi) d\omega d\lambda$$

Photoionisation	Absorptionsquerschnitt	Quantenausbeute	Wellenlängen
$O_2 + h\nu \rightarrow 2O(^1P)$	Mitschewer et al. (1992)	QA = 1	175 – 240 nm B1
$O_2 + h\nu \rightarrow O(^1P) + O_2$	DeMore et al. (1994), Farr and Bass (1985)	DeMore et al. (1994)	175 – 350 nm B2
$O_2 + h\nu \rightarrow O(^1D) + O_2$	DeMore et al. (1994) Farr and Bass (1985)	a) DeMore et al. (1994) b) Ball et al. (1994) c) Michelson et al. (1994)	175 – 320 nm B3 175 – 325 nm 175 – 325 nm
$H_2O + h\nu \rightarrow OH + H$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	175 – 189 nm
$H_2O_2 + h\nu \rightarrow 2 OH$	DeMore et al. (1994)	QA = 1	180 – 350 nm B4
$CH_3O + h\nu \rightarrow HCO + H$	a) DeMore et al. (1994) b) Müller (1991)	DeMore et al. (1994)	300 – 358 nm B5 225 – 376 nm
$CH_3O + h\nu \rightarrow CO + H_2$	a) DeMore et al. (1994) b) Müller (1991)	DeMore et al. (1994)	300 – 358 nm B5 225 – 376 nm
$CH_3CHO + h\nu \rightarrow CH_3 + CO$	Johnson et al. (1992)	Johnson et al. (1992)	260 – 295 nm B6
$CH_3CHO + h\nu \rightarrow CH_3 + HCO$	Johnson et al. (1992)	Johnson et al. (1992)	260 – 330 nm B6
$CH_3O_2H + h\nu \rightarrow CH_3O_2 + \text{Produkte}$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	210 – 300 nm
$CH_3O_2NO_2 + h\nu \rightarrow \text{Produkte}$	Johnson et al. (1992)	Johnson et al. (1992)	260 – 325 nm
$NO + h\nu \rightarrow N(^1D) + O(^1P)$	Mitschewer and DePaul (1993)	Mitschewer and DePaul (1993)	181 – 192 nm B7
$NO_2 + h\nu \rightarrow NO + O(^1P)$	a) DeMore et al. (1994) b) Schneider et al. (1987)	DeMore et al. (1994)	202 – 423 nm B8 554 – 641 nm B9
$NO_2 + h\nu \rightarrow NO_2 + O(^1P)$	Wayne et al. (1991)	Wayne et al. (1991)	400 – 641 nm B9
$N_2O + h\nu \rightarrow N_2 + O(^1D)$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	175 – 240 nm B10
$N_2O + h\nu \rightarrow N_2 + \text{Produkte}$	Wayne et al. (1991)	QA = 1 <sup>1</sup>	200 – 380 nm B11
$HONO + h\nu \rightarrow OH + NO$	Bongartz et al. (1991) <sup>1</sup>	QA = 1	300 – 399 nm
$HNO_2 + h\nu \rightarrow OH + NO_2$	Burkholder et al. (1993) <sup>1</sup>	QA = 1	180 – 350 nm B12
$HNO_2 + h\nu \rightarrow OH + NO_2$	a) DeMore et al. (1994) b) Singer et al. (1989)	DeMore et al. (1994) QA = 0.5 <sup>1</sup>	180 – 325 nm B13 190 – 320 nm
$HNO_2 + h\nu \rightarrow NO_2 + OH$	a) DeMore et al. (1994)	QA = 0.33 <sup>1</sup>	190 – 325 nm B13 <sup>1</sup>

<sup>1</sup>Amplifikation von [DeMore et al. (1994)]

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$Cl_2 + h\nu \rightarrow 2 Cl$	Singer et al. (1989)	QA = 1	190 – 320 nm
$ClO + h\nu \rightarrow Cl + O(^1P)$	Marie et al. (1993) <sup>1</sup>	QA = 1	250 – 500 nm
$ClO_2 + h\nu \rightarrow Cl + O(^1P)$	Simon et al. (1998)	QA = 1	237 – 312 nm B14
$ClO_2 + h\nu \rightarrow Cl + O(^1P)$	Wahner et al. (1987) <sup>1</sup>	QA = 1	242 – 473 nm B15
$ClO + h\nu \rightarrow Cl + O(^1P)$	DeMore et al. (1994)	QA = 1	220 – 280 nm
$Cl_2O + h\nu \rightarrow Cl + ClO$	Simon (1989) DeMore et al. (1994)	QA = 0.75 <sup>1</sup>	237 – 500 nm B16
$Cl_2O + h\nu \rightarrow Cl_2 + O(^1P)$	Simon (1989)	QA = 0.25 <sup>1</sup>	237 – 500 nm B16
$ClONO_2 + h\nu \rightarrow Cl + ClONO$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	190 – 450 nm
$HOCl + h\nu \rightarrow OH + Cl$	DeMore et al. (1994)	QA = 1	200 – 380 nm B17 <sup>1</sup>
$HO_2 + h\nu \rightarrow H + O_2$	DeMore et al. (1994)	QA = 1	175 – 220 nm
$ClONO_2 + h\nu \rightarrow Cl + \text{Produkte}$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	235 – 400 nm
$ClNO_2 + h\nu \rightarrow Cl + \text{Produkte}$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	190 – 370 nm
$ClONO_2 + h\nu \rightarrow Cl + NO_2$	a) Burkholder et al. (1994) <sup>1</sup> b) DeMore et al. (1992)	QA = 0.33 <sup>1</sup>	190 – 432 nm B18
$ClONO_2 + h\nu \rightarrow O(^1P) + ClONO$	a) Burkholder et al. (1994) <sup>1</sup> b) DeMore et al. (1992)	QA = 0.1 <sup>1</sup>	196 – 432 nm B18
$CCl_4 + h\nu \rightarrow Cl + \text{Produkte}$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	175 – 275 nm
$CCl_3F + h\nu \rightarrow Cl + \text{Produkte}$	DeMore et al. (1994)	QA = 1 <sup>1</sup>	175 – 260 nm
$BrCl + h\nu \rightarrow Br + Cl$	Marie et al. (1994)	QA = 1	260 – 600 nm B19
$Br_2 + h\nu \rightarrow 2 Br$	Marie et al. (1994)	QA = 1	200 – 650 nm B19
$HO + h\nu \rightarrow H + O(^1P)$	Wahner et al. (1989)	QA = 1	312 – 388 nm B20
$BrONO_2 + h\nu \rightarrow \text{Produkte}$	a) DeMore et al. (1994)	QA = 1	180 – 390 nm B21
$HO_2 + h\nu \rightarrow \text{Produkte}$	c) Burkholder et al. (1995)	QA = 1	209 – 509 nm
$HOBr + h\nu \rightarrow Br + OH$	a) Orlando and Burkholder (1995) b) DeMore et al. (1996)	QA = 1	196 – 432 nm B22 208 – 444 nm
$HOBr + h\nu \rightarrow Br + OH$	a) Orlando and Burkholder (1995) b) DeMore et al. (1996)	QA = 1	247 – 389 nm B23 242 – 401 nm
$HOBr_2 + h\nu \rightarrow \text{Produkte}$	DeMore et al. (1996)	QA = 1	240 – 510 nm
$Br + h\nu \rightarrow Br + O(^1P)$	Hannemann (1997)	QA = 1	371 – 480 nm B24
$Br + h\nu \rightarrow Br + O(^1P)$	Hannemann (1997)	QA = 1	338 – 472 nm
$ClO + h\nu \rightarrow \text{Produkte}$	Hannemann (1997)	QA = 1	480 – 667 nm B24

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$O_2 + h\nu$	$\rightarrow$	$2 O$	$2.44(-10)$
$O_3 + h\nu (\lambda < 325 \text{ nm})$	$\rightarrow$	$O(^1D) + O_2$	$9.46(-04)$
$O_3 + h\nu$	$\rightarrow$	$O(^1P) + O_2$	$6.53(-04)$
$O(^1P) + O_2 + M$	$\rightarrow$	$O_3 + M$	$7.98(-17)$
$O(^1D) + O_2$	$\rightarrow$	$2 NO_2$	$2.28(-15)$
$O(^1D) + O_2$	$\rightarrow$	$O(^1P) + O_2$	$4.22(-11)$
$O(^1D) + N_2$	$\rightarrow$	$O(^1P) + N_2$	$2.78(-11)$
$O(^1D) + H_2O$	$\rightarrow$	$2 OH$	$2.2(-10)$
$O(^1D) + H_2$	$\rightarrow$	$OH + H$	$1.0(-10)$
$O(^1D) + CH_4$	$\rightarrow$	$OH + CH_3(^*)$	$1.5(-10)$
$H + O_2 + M$	$\rightarrow$	$HO_2 + M$	$6.52(-15)$
$H + O_3$	$\rightarrow$	$OH + O_2$	$2.17(-11)$
$H + HO_2$	$\rightarrow$	$2 OH$	$7.3(-11)$
$H + HO_2$	$\rightarrow$	$H_2O + O(^1P)$	$1.6(-12)$
$H + HO_2$	$\rightarrow$	$H_2 + O_2$	$6.5(-12)$
$OH + O_3$	$\rightarrow$	$HO_2 + O_2$	$3.86(-14)$
$OH + HO_2$	$\rightarrow$	$H_2O + O_2$	$1.29(-10)$
$OH + H_2$	$\rightarrow$	$H_2O + H$	$1.99(-15)$
$OH + O(^1P)$	$\rightarrow$	$O_2 + H$	$3.54(-11)$

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$OH + OH$	$\rightarrow$	$H_2O + O(^1P)$	$1.62(-12)$
$HO_2 + HO_2$	$\rightarrow$	$OH + O_2$	$1.52(-15)$
$HO_2 + HO_2$	$\rightarrow$	$H_2O_2 + O_2$	$2.48(-12)$
$HO_2 + O(^1P)$	$\rightarrow$	$OH + O_2$	$6.63(-11)$
$H_2O_2 + h\nu$	$\rightarrow$	$2 OH$	$3.24(-05)$
$H_2O_2 + OH$	$\rightarrow$	$H_2O + HO_2$	$1.54(-12)$
$H_2O_2 + O(^1P)$	$\rightarrow$	$OH + HO_2$	$5.05(-16)$
$H_2O + h\nu$	$\rightarrow$	$H + OH$	$2.18(-10)$
$CO_2 + CO$	$\rightarrow$	$CO_2 + H$	$1.50(-13)$
$OH + CH_4$	$\rightarrow$	$H_2O + CH_3(^*)$	$2.11(-15)$
$NO + h\nu$	$\rightarrow$	$N + O(^1P)$	$1.40(-07)$
$N_2O + h\nu$	$\rightarrow$	$N_2 + O(^1D)$	$2.64(-07)$
$N_2O + O(^1D)$	$\rightarrow$	$2 NO$	$6.7(-11)$
$N_2 + O_2$	$\rightarrow$	$N_2 + O_2$	$4.9(-11)$
$N + O_2$	$\rightarrow$	$NO + O(^1P)$	$9.53(-18)$
$N + NO$	$\rightarrow$	$N_2 + O(^1P)$	$3.12(-11)$
$N + NO_2$	$\rightarrow$	$N_2O + O(^1P)$	$1.39(-11)$
$NO + O_3$	$\rightarrow$	$NO_2 + O_2$	$7.78(-15)$
$NO + HO_2$	$\rightarrow$	$NO_2 + OH$	$9.97(-12)$
$NO + NO_3$	$\rightarrow$	$2 NO_2$	$2.94(-11)$
$NO_2 + h\nu$	$\rightarrow$	$NO + O(^1P)$	$1.35(-02)$
$NO_2 + O_3$	$\rightarrow$	$NO_3 + O_2$	$7.28(-18)$
$NO_2 + O(^1P)$	$\rightarrow$	$NO + O_2$	$1.05(-11)$
$NO_2 + OH + M$	$\rightarrow$	$HNO_3 + M$	$3.56(-13)$
$NO_2 + NO_3 + M$	$\rightarrow$	$N_2O_5 + M$	$2.19(-13)$
$N_2O_5 + M$	$\rightarrow$	$NO_2 + NO_3 + M$	$9.42(-06)$
$HNO_3 + H_2O + M$	$\rightarrow$	$HNO_3 + M$	$2.57(-14)$
$HNO_3 + M$	$\rightarrow$	$NO_2 + HO_2 + M$	$2.12(-06)$

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$NO_3 + h\nu$	$\rightarrow$	$NO_2 + O(^1P)$	$2.56(-01)$
$NO_3 + h\nu$	$\rightarrow$	$NO + O_2$	$3.17(-02)$
$NO_3 + OH$	$\rightarrow$	$HO_2 + NO_2$	$2.2(-11)$
$NO_3 + HO_2$	$\rightarrow$	$OH + NO_2$	$3.5(-12)$
$N_2O_5 + h\nu$	$\rightarrow$	$NO_2 + NO_2$	$2.44(-04)$
$HNO_3 + h\nu$	$\rightarrow$	$NO_2 + OH$	$4.84(-05)$
$HNO_3 + OH$	$\rightarrow$	$NO_3 + H_2O$	$1.65(-13)$
$HNO_3 + h\nu$	$\rightarrow$	$NO_2 + HO_2$	$8.13(-05)$
$HNO_3 + OH$	$\rightarrow$	$NO_2 + H_2O + O_2$	$5.86(-12)$
$Cl + O_3$	$\rightarrow$	$ClO + O_2$	$1.04(-11)$
$Cl + H_2$	$\rightarrow$	$HCl + H$	$4.07(-15)$
$Cl + HO_2$	$\rightarrow$	$HCl + O_2$	$3.53(-11)$
$Cl + HO_2$	$\rightarrow$	$ClO + OH$	$6.89(-12)$
$Cl + CH_4$	$\rightarrow$	$HCl + CH_3(^*)$	$4.28(-14)$
$Cl + ClO_2$	$\rightarrow$	$2 ClO$	$6.41(-11)$
$Cl + Cl_2O_2$	$\rightarrow$	$Cl_2 + Cl + O_2$	$1.0(-10)$
$Cl + HOCl$	$\rightarrow$	$Cl_2 + OH$	$1.49(-12)$
$Cl + ClONO_2$	$\rightarrow$	$Cl_2 + NO_2$	$1.28(-11)$
$Cl_2 + h\nu$	$\rightarrow$	$2 Cl$	$3.88(-03)$
$Cl_2 + OH$	$\rightarrow$	$HOCl + Cl$	$3.95(-14)$
$ClO + O(^1P)$	$\rightarrow$	$Cl + O_2$	$3.96(-11)$

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$ClO + OH$	$\rightarrow$	$Cl + HO_2$	$1.77(-11)$
$ClO + HO_2$	$\rightarrow$	$HOCl + O_2$	$7.7(-12)$
$ClO + NO$	$\rightarrow$	$Cl + NO_2$	$2.02(-11)$
$ClO + NO_2 + M$	$\rightarrow$	$ClONO_2 + M$	$2.74(-14)$
$ClO + ClO + M$	$\rightarrow$	$Cl_2O_2 + M$	$3.2(-15)$
$Cl_2O_2 + M$	$\rightarrow$	$ClO + ClO + M$	$2.19(-03)$
$Cl_2O_2 + h\nu$	$\rightarrow$	$Cl + ClO(O^1P)$	$3.44(-03)$
$ClO + ClO$	$\rightarrow$	$ClO + O(^1P)$	$1.30(-01)$
$HOCl + h\nu$	$\rightarrow$	$Cl + OH$	$4.77(-04)$
$HOCl + OH$	$\rightarrow$	$ClO + H_2O$	$4.14(-13)$
$HOCl + O(^1P)$	$\rightarrow$	$ClO + OH$	$5.78(-14)$
$ClNO_2 + h\nu$	$\rightarrow$	$Cl + NO_2$	$9.52(-04)$
$ClONO_2 + h\nu$	$\rightarrow$	$Cl + NO_2$	$2.14(-04)$
$HCl + h\nu$	$\rightarrow$	$Cl + H$	$2.22(-07)$
$HCl + OH$	$\rightarrow$	$Cl + H_2O$	$6.49(-13)$
$Br + O_2$	$\rightarrow$	$BrO + O_2$	$1.34(-13)$
$Br + HO_2$	$\rightarrow$	$HOBr + O_2$	$1.39(-12)$
$Br + O(^1P)$	$\rightarrow$	$Br + O_2$	$4.76(-11)$
$BrO + HO_2$	$\rightarrow$	$HOBr(^*) + O_2$	$4.5(-11)$
$Br + NO_2$	$\rightarrow$	$Br + NO_2$	$2.47(-11)$
$BrONO_2 + M$	$\rightarrow$	$BrONO_2 + M$	$7.33(-14)$
$Br + ClO$	$\rightarrow$	$Br + ClO$	$8.8(-12)$
$BrO + ClO$	$\rightarrow$	$Br + Cl + O_2$	$6.94(-12)$
$BrO + ClO$	$\rightarrow$	$Br + Cl + O_2$	$1.14(-12)$
$BrO + BrO$	$\rightarrow$	$Br + Br + O_2$	$1.88(-12)$
$HOBr + OH$	$\rightarrow$	$Br + H_2O$	$1.1(-11)$
$BrCl + h\nu$	$\rightarrow$	$Br + Cl$	$1.57(-02)$
$BrONO_2 + h\nu$	$\rightarrow$	$BrO + NO_2$	$2.42(-03)$

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**Recommended Set of Equation for Stratospheric Modelling** Lecture 4: Numerical Formulation, page 25

p = 3.11 mbar, T = 252.3 K. Photolysis frequency for SZA=60°, h=39.63 km.

CH <sub>2</sub> O + hv	→	CO + H <sub>2</sub>	8.17(-05)
CH <sub>2</sub> O + hv	→	HCO + H	6.53(-05)
CH <sub>2</sub> O + OH	→	H <sub>2</sub> O + HCO	1.0(-11)
CH <sub>2</sub> O + Cl	→	HCl + HCO	7.19(-11)
CH <sub>2</sub> O + Br	→	HBr + HCO	7.14(-13)
HCO + O <sub>2</sub>	→	CO + HO <sub>2</sub>	6.1(-12)
CH <sub>3</sub> OH + OH	→	H <sub>2</sub> O + CH <sub>2</sub> O + H	6.21(-13)
CH <sub>3</sub> OH + Cl	→	HCl + CH <sub>2</sub> O + H	5.4(-11)
CH <sub>3</sub> O + HO <sub>2</sub>	→	CH <sub>3</sub> O <sub>2</sub> H + O <sub>2</sub>	9.05(-12)
CH <sub>3</sub> O <sub>2</sub> + NO	→	CH <sub>3</sub> O + NO <sub>2</sub>	8.57(-12)
CH <sub>3</sub> O + O <sub>2</sub>	→	CH <sub>2</sub> O + HO <sub>2</sub>	1.10(-15)
CH <sub>3</sub> O <sub>2</sub> + NO <sub>2</sub> + M	→	CH <sub>3</sub> O <sub>2</sub> NO <sub>2</sub> + M	2.23(-13)
CH <sub>3</sub> O <sub>2</sub> NO <sub>2</sub> + M	→	CH <sub>3</sub> O <sub>2</sub> + NO <sub>2</sub> + M	9.04(-05)
CH <sub>3</sub> O <sub>2</sub> + ClO	→	Cl + CH <sub>2</sub> O + HO <sub>2</sub>	1.33(-12)
CH <sub>3</sub> O <sub>2</sub> + CH <sub>3</sub> O <sub>2</sub>	→	CH <sub>2</sub> O + CH <sub>3</sub> OH + O <sub>2</sub>	3.19(-13)
CH <sub>3</sub> O <sub>2</sub> H + hv	→	CH <sub>2</sub> O + OH + H	2.09(-05)
CH <sub>3</sub> O <sub>2</sub> H + OH	→	CH <sub>3</sub> O <sub>2</sub> + H <sub>2</sub> O	5.88(-12)
CH <sub>3</sub> O <sub>2</sub> H + OH	→	CH <sub>2</sub> O + OH + H <sub>2</sub> O	2.52(-12)
CH <sub>3</sub> O <sub>2</sub> H + Cl	→	HCl + CH <sub>2</sub> O + OH	6.41(-11)
CH <sub>3</sub> O <sub>2</sub> NO <sub>2</sub> + hv	→	CH <sub>3</sub> O <sub>2</sub> + NO <sub>2</sub>	1.05(-04)

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**Set of Ordinary Differential Equation for Chemical Models** Lecture 4: Numerical Formulation, page 26

Determination of C<sub>i</sub> (Determination of chemical loss and production rates)

$$C_i = \frac{d[y_i]}{dt} = P_i - L_i[y_i]$$

$$P_i = \sum_{j=1, j \neq i} k_{ji}[j][l] + \sum_{m=1} j_m[m]$$

$$L_i = \sum_j k_{ij}[j] + k_i$$

*k<sub>ji</sub> : reaction coefficients*

*j<sub>m</sub> : photolysis rates*

**Different chemical reactions**

- bi-molecular
- tri-molecular
- thermal
- heterogeneous
- photolysis

Determination of C<sub>i</sub> implies simultaneous solution of up to hundreds of coupled differential equations, containing many non-linear reactions.

Set of stiff differential equations => Numerical Solution difficult

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**ODEs and PDEs** Lecture 4: Numerical Formulation, page 27

**Ordinary differential equation (ODE)**  
Equation with one independent variable

**Partial differential equation (PDE)**  
Equation with more than one independent variable

**Order**  
Highest derivative of an equation

**Degree**  
Highest polynomial value of the highest derivative

**Initial value problem**  
Conditions are known at one end of domain but not other

**Boundary value problem**  
Conditions are known at both ends of domain

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**ODEs and PDEs** Lecture 4: Numerical Formulation, page 28

	Ordinary Differential Equations	Partial Differential Equations
<b>First-order, first-degree</b>	(a) $\frac{dN}{dt} = 16 - 4N^2$	(e) $\frac{\partial N}{\partial t} + \frac{\partial(uN)}{\partial x} = 0$
<b>First-order, first-degree</b>	(b) $\frac{dN}{dt} = 3AB - 4NC$	(f) $\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = 0$
<b>Second-order, first-degree</b>	(c) $\frac{d^2 N}{dt^2} + \frac{dN}{dt} + 5t = 0$	(g) $\frac{\partial^2 N}{\partial t^2} + \frac{\partial^2 N}{\partial x^2} = 3t^2 + x$
<b>Second-order, second-degree</b>	(d) $\left(\frac{d^2 N}{dt^2}\right)^2 + \frac{dN}{dt} + 4 = 0$	(h) $\left(\frac{\partial^2 N}{\partial t^2}\right)^2 + \frac{\partial N}{\partial x} = t - x$

Deutsches Zentrum für Luft- und Raumfahrt e.V. in der Helmholtz-Gemeinschaft Source: Jacobson, Fundamentals of Atmospheric Modeling

**Operator Splitting Scheme** Lecture 4: Numerical Formulation, page 29

**Major processes in an atmospheric model are often solved separately from each other**  
Suppose a model has dynamics, transport, radiation and gas chemistry  
Each of these processes may be solved sequentially during a common time interval

**Time step**  
is an increment in time for a given process

**Time interval**  
is the period during which several time steps of a process are solved

**Example**  
time dynamics 15 min, transport 15 min, radiation 45 min (every 3 time steps), chemistry variable, time interval common to all is 45 min => during the time interval 3 dynamics and transport time steps are taken, followed by 1 radiation time step, followed by a variable number of chemistry time steps; after the dynamics time interval, resulting wind speeds are taken as input for transport calculations; during the transport interval gases are moved around in the grid; this is input for the chemistry calculations, and radiation.

Time interval 1

Dynamics, Transport

Radiation

Chemistry

Time interval 2

Dynamics, Transport

Radiation

Chemistry

Modified from Fig. 6.1 Source: Jacobson, Fundamentals of Atmospheric Modeling

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**Differences GCM and NWP models** Lecture 4: Numerical Formulation, page 30

- Major difference between **GCM** and **NWP model**: climate model is used to project the average behaviour of the atmosphere (its climate) as a result of **slow changes in some boundary conditions** (such as the solar constant) or **physical parameters** (such as the greenhouse gas concentration) and **not to make a deterministic prediction of the exact weather at a specific time**.
- A chaotic nature of the fluid dynamics equations is involved in weather forecasting. Extremely small errors in temperature, winds, or other initial inputs given to numerical models will amplify and double every five days, making it impossible for long-range forecasts—those made more than two weeks in advance—to predict the state of the atmosphere with any degree of forecast skill. Furthermore, existing observation networks have poor coverage in some regions (e.g., over Pacific Ocean), which introduces uncertainty into the true initial state.
- The unpredictable, chaotic nature of the atmosphere means that **deterministic predictions are not possible**. However, it is possible to **predict changes in climate due to changes in boundary conditions**, such as exchanges with the ocean or the land surface, or changes in external forcing factors, such as changes in solar radiation or GHGs.
- NWP models are used to predict the weather in the **short (1-3 days)** and **medium (4-10 days)** range future. GCM's are run much longer, for years on end, long enough to learn about the **climate in a statistical sense** (i.e. trends, means and variability).
- GCMs ignore fluctuating conditions when considering long-term changes, whereas NWP models take no notice of very slow processes.

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**A comparison between NWP models and GCMs** Lecture 4: Numerical Formulation, page 31

contrasts	NWP	GCM
goal	to predict weather	to predict climate
spatial coverage	regional or global	global
temporal range	days	years
spatial resolution	variable (20-100 km)	usually coarse
relevance of initial conditions	high	low
relevance of clouds, radiation	low	high
relevance of surface (land, ice, ocean...)	low	high
relevance of ocean dynamics	low	high
relevance of model stability	low	high
similarities		
physics	equations of motion (plus radiative transfer equations, water conservation equations...)	
method	Finite difference expression of continuous equations, or spectral representation; run prognostically	

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Lecture 4: Numerical Formulation, page 32

# Methods to solve differential equations

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**Finite Difference Approximation** Lecture 4: Numerical Formulation, page 33

First, replace continuous function  $u_i$  with a finite number of values in the  $x$  direction.  
Second, define differences of  $u$  at point  $x_i$

$\rightarrow \Delta u_i = u_{i+1} - u_{i-1}$     central difference  
 $\rightarrow \Delta u_i = u_{i+1} - u_i$     forward difference  
 $\rightarrow \Delta u_i = u_i - u_{i-1}$     backward difference

Central difference approximation to tangent slope at  $x_i$

$$\frac{\partial u}{\partial x} \approx \frac{\Delta u_i}{\Delta x_i} = \frac{u_{i+1} - u_{i-1}}{x_{i+1} - x_{i-1}}$$

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Source: Jacobsen, Fundamentals of Atmospheric Modelling

**Taylor Series Expansion** Lecture 4: Numerical Formulation, page 34

Taylor series expansion of concentration  $N$  at point  $x+\Delta x$  (6.11)

$$N_{x+\Delta x} = N_x + \Delta x \frac{\partial N_x}{\partial x} + \frac{1}{2} \Delta x^2 \frac{\partial^2 N_x}{\partial x^2} + \frac{1}{6} \Delta x^3 \frac{\partial^3 N_x}{\partial x^3} + \frac{1}{24} \Delta x^4 \frac{\partial^4 N_x}{\partial x^4} + \dots$$

Taylor series expansion of concentration  $N$  at point  $x-\Delta x$  (6.12)

$$N_{x-\Delta x} = N_x - \Delta x \frac{\partial N_x}{\partial x} + \frac{1}{2} \Delta x^2 \frac{\partial^2 N_x}{\partial x^2} - \frac{1}{6} \Delta x^3 \frac{\partial^3 N_x}{\partial x^3} + \frac{1}{24} \Delta x^4 \frac{\partial^4 N_x}{\partial x^4} - \dots$$

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Source: Jacobsen, Fundamentals of Atmospheric Modelling

**Finite Difference Approximations** Lecture 4: Numerical Formulation, page 35

Sum the Taylor series expansions (6.13)

$$N_{x+\Delta x} + N_{x-\Delta x} = 2N_x + \Delta x^2 \frac{\partial^2 N_x}{\partial x^2} + \frac{1}{12} \Delta x^4 \frac{\partial^4 N_x}{\partial x^4} + \dots$$

Rearrange (6.14)

$$\frac{\partial^2 N_x}{\partial x^2} = \frac{N_{x+\Delta x} - 2N_x + N_{x-\Delta x}}{\Delta x^2} + O(\Delta x^2)$$

Truncation error (neglect 2<sup>nd</sup>-order terms and higher) (6.15)

$$O(\Delta x^2) = -\frac{1}{12} \Delta x^2 \frac{\partial^4 N_x}{\partial x^4} - \dots$$

2<sup>nd</sup>-order central difference approx. of 2<sup>nd</sup> derivative (6.16)

$$\frac{\partial^2 N_x}{\partial x^2} \approx \frac{N_{x+\Delta x} - 2N_x + N_{x-\Delta x}}{\Delta x^2}$$

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Source: Jacobsen, Fundamentals of Atmospheric Modelling

**Finite Difference Approximations** Lecture 4: Numerical Formulation, page 36

Subtract the Taylor series expansions (6.17)

$$N_{x+\Delta x} - N_{x-\Delta x} = 2\Delta x \frac{\partial N_x}{\partial x} + \frac{1}{3} \Delta x^3 \frac{\partial^3 N_x}{\partial x^3} + \dots$$

Rearrange (6.18)

$$\frac{\partial N_x}{\partial x} = \frac{N_{x+\Delta x} - N_{x-\Delta x}}{2\Delta x} + O(\Delta x^2)$$

Truncation error (6.19)

$$O(\Delta x^2) = -\frac{1}{6} \Delta x^2 \frac{\partial^3 N_x}{\partial x^3} - \dots$$

2<sup>nd</sup>-order central difference approx. of 1<sup>st</sup> derivative (6.20)

$$\frac{\partial N_x}{\partial x} \approx \frac{N_{x+\Delta x} - N_{x-\Delta x}}{2\Delta x} = \frac{N_{i+1} - N_{i-1}}{2\Delta x}$$

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Source: Jacobsen, Fundamentals of Atmospheric Modelling

First two terms of Taylor series

1<sup>st</sup>-order forward difference approx. of 1<sup>st</sup> derivative (6.21)

$$\frac{\partial N_x}{\partial x} \approx \frac{N_{x+\Delta x} - N_x}{\Delta x} = \frac{N_{i+1} - N_i}{\Delta x}$$

1<sup>st</sup>-order backward difference approx. of 1<sup>st</sup> derivative (6.22)

$$\frac{\partial N_x}{\partial x} \approx \frac{N_x - N_{x-\Delta x}}{\Delta x} = \frac{N_i - N_{i-1}}{\Delta x}$$

Central, forward, backward difference approximations (6.23)

$$\frac{\partial N_t}{\partial t} \approx \frac{N_{t+h} - N_{t-h}}{2h}$$

$$\frac{\partial N_t}{\partial t} \approx \frac{N_{t+h} - N_t}{h}$$

$$\frac{\partial N_t}{\partial t} \approx \frac{N_t - N_{t-h}}{h}$$

A numerical solution can replicate an exact solution to a PDE if several criteria are met:

Convergence of finite difference analog (6.6)

$$\frac{\partial N}{\partial x} = \lim_{\Delta x \rightarrow 0} \left| \frac{\Delta N}{\Delta x} \right|$$

Consistency of finite difference analog (6.7)

$$\lim_{\Delta x \rightarrow 0} \left\| \text{T.E.} \left( \frac{\Delta N}{\Delta x} \right) \right\| = 0$$

Convergence of overall solution ( $N_e$ : exact solution;  $N_f$ : finite-difference solution) (6.8)

$$\lim_{\Delta x, \Delta t \rightarrow 0} \|N_{e,x,t} - N_{f,x,t}\| = 0$$

Stability occurs if the absolute-value difference between the numerical and the exact solution does not grow over time (often depends on the time step used).

Stability  $\lim_{t \rightarrow \infty} \|N_{e,x,t} - N_{f,x,t}\| \leq C$  (6.9)

Conditionally stable: Stable for limited time-step range

Unconditionally stable: Stable for all time steps

Unconditionally unstable: Unstable for all time steps

An unconditionally unstable scheme cannot be convergent overall, but individual finite-difference analogs in an unstable scheme may converge and may be consistent.

In other words, consistency and convergence of individual analogs do not guarantee stability.

Stability is guaranteed if a scheme is convergent overall and its finite-difference analogs are convergent and consistent.

- Sets of chemical lifetimes of species vary by many orders of magnitude
- The analysis of stiff circuits requires the use of variable step sizes
- Not all the linear multistep methods can be efficiently used to integrate stiff equations

To be able to choose  $\Delta t$  based only on accuracy considerations, the region of absolute stability should allow a large  $\Delta t$  for large time constants, without being constrained by the small time constants

See further details for example in Sandu & Sander, 2006

### Stable

If the absolute-value difference between the numerical and the exact solution does not grow with time

### Accurate

Check time-dependent solution from the solver with an exact solution

### Mass-conserving

A scheme is mass-conserving if the mass of each element (e.g. N, O, H, etc.) summed over all species at the beginning of the simulation equals the mass of the element summed over all species at the end of the simulation

### Positive definite

If a scheme always predicts non-negative concentrations

### Fast

A good solver can take long time-steps and maintain accuracy

Methods for the chemical part Lecture 4: Numerical Formulation, page 43

- **Analytical solution**
- **Classical numerical methods for stiff ODEs**
  - Taylor series solution
  - Forward-Euler Solution
  - Multi-step implicit Solution
  - Backward-Euler Solution
  - Gear's Method
  - Implicit and semi-implicit methods
  - Family Solution

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Initial Value Problems Lecture 4: Numerical Formulation, page 44

Values are known at an initial time and desired at a final time

Concentration of species  $i$  is known at time  $t-h=0$  (12.2)

$$N_{i,t-h} = N_{i,0}$$

Vector of concentrations at time  $t$  for a set of  $K$  species (12.1)

$$\hat{N}_t = [N_{1,t}, N_{2,t}, \dots, N_{i,t}, \dots, N_{K,t}]$$

- During a time step, an ODE scheme solves for all  $N_{i,t}$
- Once values at time  $t$  are found,  $t$  is replaced with  $t-h$  and a new time step is solved
- $h$ : one time step

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Analytical Solution to ODEs (most accurate) Lecture 4: Numerical Formulation, page 45

Nitrogen dioxide photolysis (12.4)

$$\dot{\text{NO}}_2 + h\nu \longrightarrow \dot{\text{NO}} + \dot{\text{O}} \cdot$$

Time rate of change of  $\text{NO}_2$  concentration (12.5)

$$\frac{d[\text{NO}_2]}{dt} = -J[\text{NO}_2]$$

Analytical solution (12.6)

$$[\text{NO}_2]_t = [\text{NO}_2]_{t-h} e^{-Jh}$$

Example:

$[\text{NO}_2]_{t-h}$	$= 10^{10} \text{ molec. cm}^{-3}$	<ul style="list-style-type: none"> <li>• Analytical solutions to a set of ODEs are usually impractical to obtain</li> <li>• <math>\Rightarrow</math> Numerical solutions are used in atmospheric models</li> </ul>
$J$	$= 0.02 \text{ s}^{-1}$	
$[\text{NO}_2]_t$	$= 10^{10} e^{-0.02t}$	

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Taylor Series Solution to ODEs Lecture 4: Numerical Formulation, page 46

Explicit Taylor series expansion for one species (12.7)

$$N_{i,t} = N_{i,t-h} + h \frac{dN_{i,t-h}}{dt} + \frac{h^2}{2} \frac{d^2 N_{i,t-h}}{dt^2} + \frac{h^3}{6} \frac{d^3 N_{i,t-h}}{dt^3} + \dots$$

Taylor series expansion for NO (12.8)

$$[\text{NO}]_t = [\text{NO}]_{t-h} + h \frac{d[\text{NO}]_{t-h}}{dt} + \frac{h^2}{2} \frac{d^2 [\text{NO}]_{t-h}}{dt^2} + \frac{h^3}{6} \frac{d^3 [\text{NO}]_{t-h}}{dt^3} + \dots$$

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Family Method Lecture 4: Numerical Formulation, page 47

Organize short- and long-lived species into families, which are long-lived, solve for family concentration, then partition family concentrations into individual species concentrations

Odd oxygen family (12.92)

$$[\text{O}_T] = [\text{O}] + [\text{O}(^1\text{D})] + [\text{O}_3] + [\text{NO}_2]$$

Odd hydrogen family (12.93)

$$[\text{HO}_T] = [\text{OH}] + [\text{HO}_2] + [\text{H}_2\text{O}_2]$$

Odd nitrogen family (12.94)

$$[\text{NO}_T] = [\text{NO}] + [\text{NO}_2] + [\text{NO}_3]$$

Odd chlorine family (12.95)

$$[\text{Cl}_T] = [\text{Cl}] + [\text{ClO}] + [\text{ClO}_2]$$

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## Grid and Time Resolution

- Computing power limits the amount of calculation that can occur
- Thus, calculations are performed on a "grid" of points
  - Typically  $5^\circ \times 5^\circ$  horizontal grid ( $\sim 555 \times 555$  km at the Equator)
  - Also divide the atmosphere into vertical layers
- Since we are stepping forward in time, climate models have 4 dimensions



## Model Stability

- As spatial resolution increases, the time resolution must also increase or climate models will not yield a stable solution (they will “blow up”)
  - This is called the CFL criterion, named after Courant, Friedrichs, and Lewy, and is represented mathematically as:

Fastest signal propagating through the model domain (e.g. a gravity wave in the atmosphere with a speed of 300 m/s)

$$\frac{c\Delta t}{\Delta x} \leq 1$$

\*\* Richardson used a 6 hour time step ( $\Delta x = 200$  km) in his experiment. He would have had to used a time step of 8 minutes to find a stable solution

Lecture 4: Numerical Formulation, page 50

## Steps in Model Formulation

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Steps in Model Formulation

Lecture 4: Numerical Formulation, page 51

1. Define purpose of model (e.g., simulate tropospheric climate or stratospheric ozone)
2. Determine spatial and temporal scales of interest (e.g. global and centuries)
3. Determine dimension of model (e.g., 3D)
4. Select physical, chemical, dynamical processes treated (e.g., fully coupled)
5. Select variables (e.g. 10 meteorological variables and 150 chemical species)
6. Select computer architecture (e.g., parallel-processor machine)
7. Write code for model
8. Optimize memory and speed of model (e.g., minimizing global arrays)
9. Select time steps and time intervals (e.g., 300 s for a  $5^\circ \times 5^\circ$  grid).
10. Set initial conditions (e.g., use observations or output from previous model run)
11. Set boundary conditions (e.g., set south-north velocities to 0 at poles)
12. Select input data (e.g., topography, chemical rate coefficients, absorption coefficients, emissions)
13. Select ambient observations for comparison (e.g., satellite data to judge performance)
14. Interpolate observations and model results for inputs and outputs
15. Select or write algorithms for statistics and graphics (e.g. by using NCL)
16. Run model simulations
17. Run sensitivity tests (e.g., to gauge the effect of model assumptions or processes)
18. Improve model based on results (e.g., through comparison with observations)

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Steps in Model Formulation: 1. Define purpose

Lecture 4: Numerical Formulation, page 52

For example:  
Understanding and Attributing Climate Change

Predicting the Future:  
Climate Change; Source: IPCC 2007

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Steps in Model Formulation

Lecture 4: Numerical Formulation, page 53

1. Define purpose of model (e.g., simulate tropospheric climate or stratospheric ozone)
2. Determine spatial and temporal scales of interest (e.g. global and centuries)
3. Determine dimension of model (e.g., 3D)
4. Select physical, chemical, dynamical processes treated (e.g., fully coupled)
5. Select variables (e.g. 10 meteorological variables and 150 chemical species)
6. Select computer architecture (e.g., parallel-processor machine)
7. Write code for model
8. Optimize memory and speed of model (e.g., minimizing global arrays)
9. Select time steps and time intervals (e.g., 300 s for a  $5^\circ \times 5^\circ$  grid).
10. Set initial conditions (e.g., use observations or output from previous model run)
11. Set boundary conditions (e.g., set south-north velocities to 0 at poles)
12. Select input data (e.g., topography)
13. Select ambient observations for comparison (e.g., satellite data to judge performance)
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15. Select or write algorithms for statistics and graphics (e.g. by using NCL)
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18. Improve model based on results (e.g., through comparison with observations)

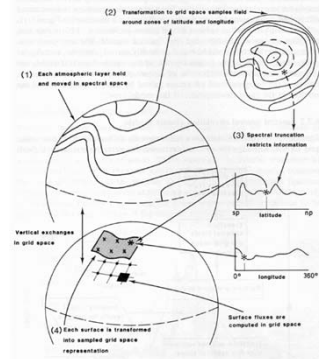
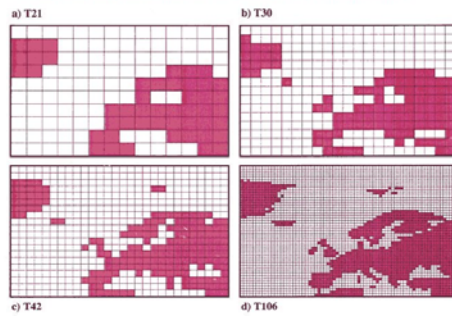
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The Atmosphere over Europe in a discrete model

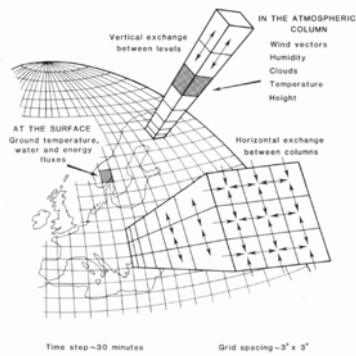
Lecture 4: Numerical Formulation, page 54

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European part of the land-sea mask for different T-model resolutions



Source: A Climate Modelling Primer, Henderson-Sellers &amp; McGuffie, Figure 6.3(b)



Source: A Climate Modelling Primer, Henderson-Sellers &amp; McGuffie, Figure 6.3(a)

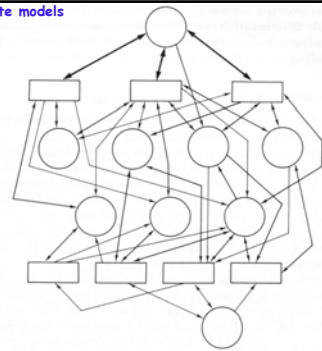
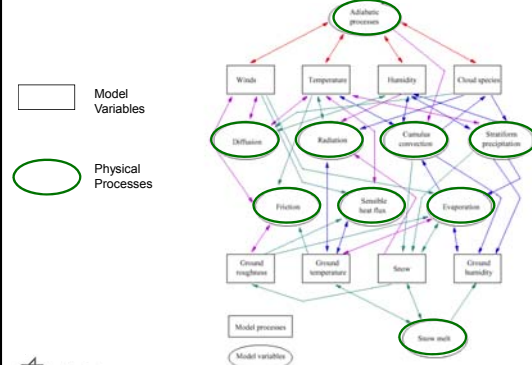
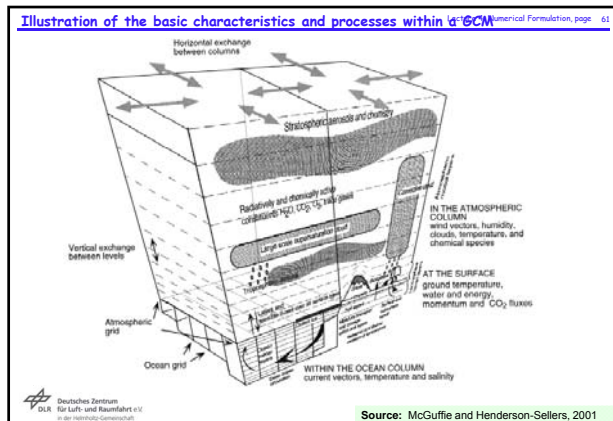


Figure 2.9 A generalized 'spaghetti' diagram for climate models. The arrows show the links between a set of unnamed processes and variables. The processes which could be entered in the boxes and the variables in the circles depend crucially on the timescale being modelled and the type of model employed.

1. Define purpose of model (e.g., simulate tropospheric climate or stratospheric ozone)
2. Determine spatial and temporal scales of interest (e.g. global and centuries)
3. Determine dimension of model (e.g., 3D)
4. Select physical, chemical, dynamical processes treated (e.g., fully coupled)
5. Select variables (e.g. 10 meteorological variables and 150 chemical species)
6. Select computer architecture (e.g., parallel-processor machine)
7. Write code for model
8. Optimize memory and speed of model (e.g., minimizing global arrays)
9. Select time steps and time intervals (e.g., 300 s for a 5°x5° grid).
10. Set initial conditions (e.g., use observations or output from previous model run)
11. Set boundary conditions (e.g., set south-north velocities to 0 at poles)
12. Select input data (e.g., topography)
13. Select ambient observations for comparison (e.g., satellite data to judge performance)
14. Interpolate observations and model results for inputs and outputs
15. Select or write algorithms for statistics and graphics (e.g. by using NCL)
16. Run model simulations
17. Run sensitivity tests (e.g., to gauge the effect of model assumptions or processes)
18. Improve model based on results (e.g., through comparison with observations)





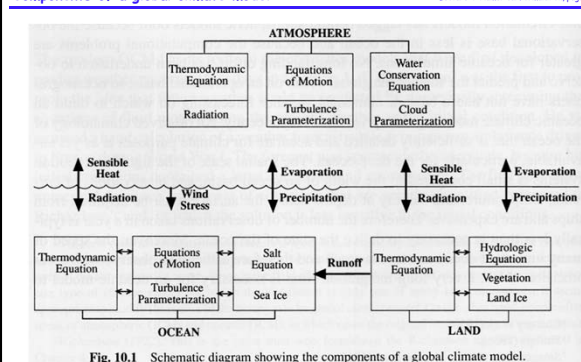
## Parameterization

- Since by necessity our grid is large, many things occur at scales smaller than the grid size
  - Clouds
- Model cannot “see” these things
- **Parameterizations** are employed to simulate the large-scale feedback that small scale features produce
  - Calculate an “average” cloudiness over a grid box

## Typical Climate Model Parameterizations

- Convection and Clouds
  - Mass, momentum, heat, moisture fluxes
  - Fluxes are usually much larger at scales smaller than a climate model grid size
  - Radiation interactions
- Turbulence
- Radiation
- Boundary Layer
  - Fluxes of heat, moisture, momentum

## Components of a global climate model



## Steps in Model Formulation

1. Define purpose of model (e.g., simulate tropospheric climate or stratospheric ozone)
2. Determine spatial and temporal scales of interest (e.g. global and centuries)
3. Determine dimension of model (e.g., 3D)
4. Select physical, chemical, dynamical processes treated (e.g., fully coupled)
5. Select variables (e.g. 10 meteorological variables and 150 chemical species)
6. Select computer architecture (e.g., parallel-processor machine)
7. Write code for model
8. Optimize memory and speed of model (e.g., minimizing global arrays)
9. Select time steps and time intervals (e.g., 300 s for a  $5^\circ \times 5^\circ$  grid).
10. **Set initial conditions (e.g., use observations or output from previous model run)**
11. **Set boundary conditions (e.g., set south-north velocities to 0 at poles)**
12. **Select input data (e.g., topography)**
13. Select ambient observations for comparison (e.g., satellite data to judge performance)
14. Interpolate observations and model results for inputs and outputs
15. Select or write algorithms for statistics and graphics (e.g. by using NCL)
16. Run model simulations
17. Run sensitivity tests (e.g., to gauge the effect of model assumptions or processes)
18. Improve model based on results (e.g., through comparison with observations)

## What do we need to start a GCM simulation?


### 1. Initial Conditions

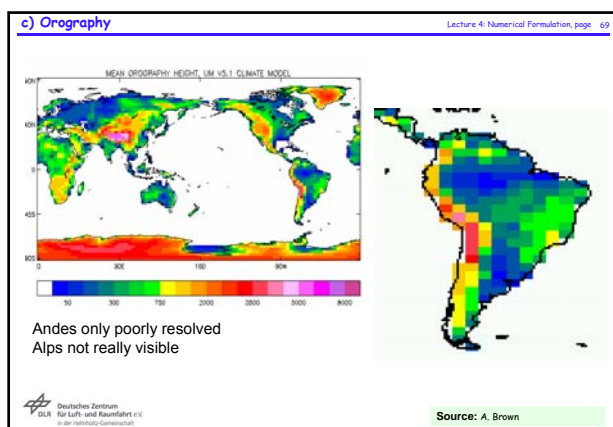
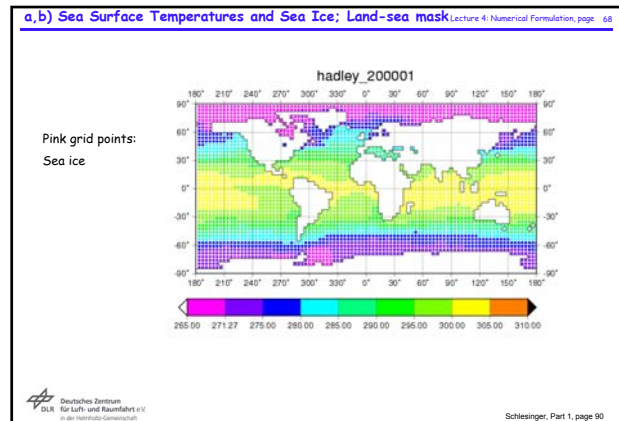
- Possible existence of multiple attractors make the choice of initial conditions far from trivial
- Possibilities for initial conditions:
  - start from stable solution (e.g. an atmosphere without horizontal gradients)
  - start close to an observed state (weather predictions, decadal simulations in CMIP5).
- Spinup: time until the simulations is independent from the initial conditions
  - depends on the application
  - short in the atmosphere due to the lack of inertia (few months)
  - processes at the land surface (in particular cumulative processes that depend on the storage of water below the ground) have a large inertia and need several years spinup
  - even longer spinup is needed if the GCM runs with a coupled ocean

What do we need to start a GCM simulation? Lecture 4: Numerical Formulation, page 67

2. Surface boundary conditions

- Sea Surface Temperatures (SSTs) and sea-ice (or a coupled ocean)
- Land-sea mask
- Orography
- Roughness length (*Sea, Sea-ice, Land*)
- Vegetation
- Albedo for different surface types
- Emissions (GHGs, CFCs, ozone precursors etc.)
- Prescribed 3D concentration for aerosols and ozone (if not interactively modeled)
- Solar forcing data
- volcanic aerosol dataset

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d) Roughness Length Lecture 4: Numerical Formulation, page 70

The **roughness length** is used in numerical models to **express the roughness of the surface**. It affects the intensity of **mechanical turbulence** and the **fluxes** of various quantities above the surface.

The 'roughness length' depends on the **frontal area of the average element** (facing the wind) **divided by the ground width it occupies**. Vertical sub-gridscale **heat exchange** (by turbulent eddies) can be expressed as the **vertical gradient of potential temperature times the roughness length**.

A **lower roughness length** implies **less exchange between the surface and the atmosphere**, but also stronger wind near the ground (e.g. at the standard height of 10 m).  
A terrain classification based on roughness length is given in the following table:


class	roughness length, m	landscape features
1 sea	0.0002	open water, tidal flat, snow with fetch above 3 km
2 smooth	0.005	featureless land, ice
3 open	0.03	flat terrain with grass or very low vegetation, airport runway
4 roughly open	0.10	cultivated area, low crops, obstacles of height H separated by at least 20 H
5 rough	0.25	open landscape, scattered shelter belts, obstacles separated by 10 H or so
6 very rough	0.5	landscape with bushes, young dense forest etc. separated by 10 H or so
7 closed	1.0	open spaces comparable with H, eg mature forest, low-rise built-up area
8 chaotic	over 2.0	irregular distribution of large elements, eg city centre, large forest with clearings

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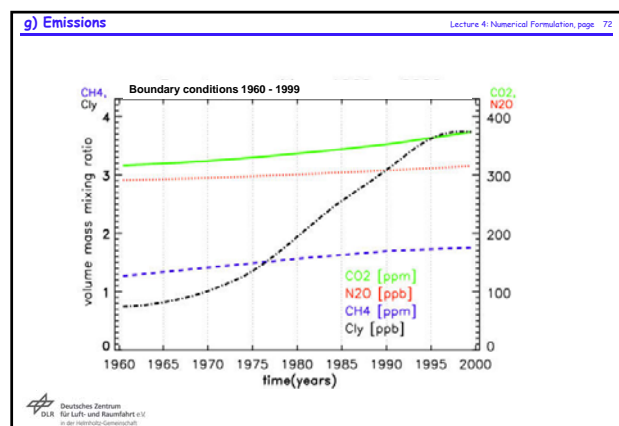
f) Typical Surface Albedos Lecture 4: Numerical Formulation, page 71

Surface type	Albedo ( $\alpha$ )
Soil, dark and wet	0.05
Soil, light and dry	0.40
Desert	0.20-0.45
Savanna grassland, wet season	0.18
Savanna grassland, dry season	0.23
Grass, long	0.16
Grass, short	0.26
Cropland	0.18-0.25
Orchards	0.15-0.20
Forest	0.05-0.20
Water, small zenith angle	0.03-0.10
Water, large zenith angle	0.10-1.00
Snow	0.40-0.95

*[note that 0.25 represents 25% of radiation reflected]*

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<http://www.giss.us.es/autocourses/GEOS210/lectures/lecture2.pdf>



Simulation design, preparation, integration, interpretation Lecture 4: Numerical Formulation, page 73

**Simulation design:**

- Choice of model configuration, including model vertical and horizontal resolution and complexity
- choice among the different subgrid scale parameterisations & parameters for it
- precise definition of the initial and boundary conditions that will be used for the experiment
- incorporate the material and personal constraints that can limit the scope of the simulation and try to find a reasonable balance between the scientific interest of the simulation and the overall costs and human and computer time.

**Preparation:**

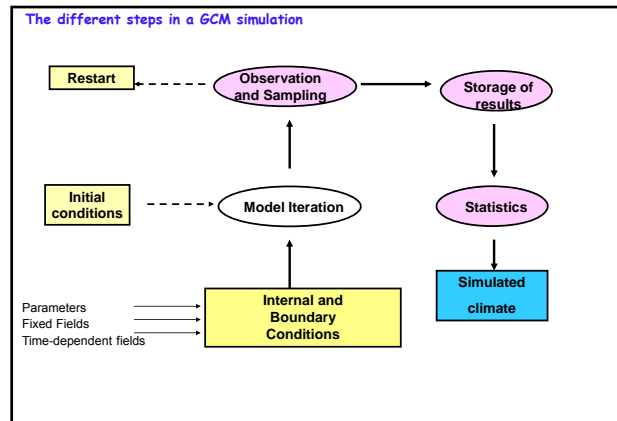
- prepare and check initial conditions and boundary conditions

**Integration:**

- start test runs (few months)
- Start run and check regularly
- Postprocess the output in order to bring out interesting results

**Interpretation:**

interpretation of the results



Short Description of the GCM ECHAM5 (1 of 8) Lecture 4: Numerical Formulation, page 75

**1.1 Short Description**

The **ECHAM** model has been developed from the **ECMWF model** (cycle 31, November 1988). It contains several changes, mostly in the parameterization, in order to adjust the model for climate simulations.

The reference resolution is T42, but the model is set up to use resolutions in the range **T21 to T106**. Long term integrations have so far only been done for T21, T30, T42 and T63. The layout is as follows (indicates changes from the original ECMWF model):

**1.2 Numerical solution**

- **Prognostic variables:** e.g., vorticity, divergence, temperature, log surface pressure, water vapour, cloud species
- **Horizontal representation:** spectral transform, triangular truncation (T42/T63/T106); in all practical applications the series expansion of spherical harmonic functions must be truncated at some finite point.
- **Vertical representation:** hybrid coordinate system, second order finite differences, 19, 39, and 69 layers
- **Time integration:** semi-implicit | leap frog with time filter,  $\tau = 40$  min (T21),  $\tau = 30$  min (T30),  $\tau = 24$  min (T42),  $\tau = 15$  min (T63), and  $\tau = 12$  min (T106)

Short Description of the GCM ECHAM5 (2 of 8) Lecture 4: Numerical Formulation, page 76

**1.3 Surface boundary conditions**

- **SST and sea-ice:** e.g. Hadley data set
- **Orography:** mean terrain heights computed from high resolution USGS GTOPO30 data set
- **Land-sea mask:** from USGS GTOPO30 data set
- **Roughness length:**
  - Sea:* Charnock formula, modified after Miller et al. (1992)
  - Sea-ice:* constant (0.01 m)
  - Land:* function of vegetation and orography (variance)
- **Vegetation:** fraction of grid area covered by vegetation based on Wilson and Henderson-Sellers (1985) data
- **Albedo:**
  - Sea:* function of solar zenith angle bare
  - Land:* satellite data (Geleyn and Preuss (1983))
  - Sea ice:* function of temperature (Robock, 1980)
  - Land ice:* function of temperature (Robock, 1980; Kukla and Robinson, 1980)
  - Snow:* function of temperature and fractional forest area (Robock, 1980; Matthews, 1983)

Short Description of the GCM ECHAM5 (3 of 8) Lecture 4: Numerical Formulation, page 77

**1.4 Physical parameterization**

**Radiation:** (Hense et al., 1982; Rockel et al., 1991; Eickerling, 1989)

- two-stream approximation
- six spectral intervals in the terrestrial part
- four spectral intervals in the solar part
- **gaseous absorbers:**  $H_2O$ ,  $CO_2$  and  $O_3$  ( $CO_2$  and  $O_3$  prescribed)
- **aerosols:** prescribed
- **clouds:** computed cloud optical depth and cloud cover
- **emissivity:** function of cloud water path (Stephens, 1978)
- **continuum absorption:** included
- **cloud overlap:** maximum for contiguous clouds layer and random otherwise
- **diurnal cycle:** included
- **radiation time step:** 2 hours

Short Description of the GCM ECHAM5 (4 of 8) Lecture 4: Numerical Formulation, page 78

**1.4 Physical parameterization**

**Clouds:** (Sundquist, 1978; Roeckner and Schlese, 1985; Roeckner et al., 1991)

**Cloud water transport equation**

**Subgrid-scale condensation and cloud formation**  
with different thresholds for convective and stratiform clouds (Xu and Krueger, 1991)

**Temperature dependent partitioning of liquid/ice phase** (Matveev, 1984)

**Rain formation** by auto-conversion of cloud droplets (Sundquist, 1978)

**Sedimentation of ice crystals** (Heymsfeld, 1977)

**Evaporation of cloud water**  
**Evaporation of precipitation**

See video on CLOUDS (EU-EUCLIPSE project) at <http://www.youtube.com/watch?v=5UCb38VzklI>

Short Description of the GCM ECHAM5 (5 of 8) Lecture 4: Numerical Formulation, page 79

**1.4 Physical parameterization**

**Convection:** (Tiedtke, 1989)


*Mass flux scheme for deep, shallow and mid-level convection*

*Clouds* are represented by a bulk model and include updraft and downdraft mass fluxes

*Convective momentum transport* is parameterized according to Schneider and Lindzen (1976)

*Evaporation of rain* is parameterized according to Kessler (1969)

*Stratocumulus convection* is parameterized as a vertical diffusion process with enhanced eddy diffusion coefficients (Tiedtke et al., 1988)

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Short Description of the GCM ECHAM5 (6 of 8) Lecture 4: Numerical Formulation, page 80

**1.4 Physical parameterization**

**Land-surface processes:** (Sellers et al., 1986; Blondin, 1989; Du'menil and Todini, 1992)

- *Heat transfer:* diffusion equation solved in a 5-layer model with zero heat flux at the bottom (10 m)
- *Water budget equation for three reservoirs:* soil moisture, interception reservoir (vegetation), snow
- *Vegetation effects:* stomatal control on evapotranspiration and interception of rain and snow
- *Run-off scheme:* based on catchment considerations including sub-grid scale variations of field capacity over inhomogeneous terrain
- *Sea-ice temperature* calculated from surface energy budget

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Short Description of the GCM ECHAM5 (7 of 8) Lecture 4: Numerical Formulation, page 81

**1.4 Physical parameterization**

**Planetary boundary layer:** (Louis, 1979)

- *Surface fluxes of momentum, heat, moisture and cloud water* are calculated from Monin-Obukhov similarity theory with transfer coefficients depending on roughness length and Richardson number
- *Above the surface layer:* eddy diffusivity approach with coefficients depending on wind shear, thermal stability and mixing length
- *Above the PBL:* vertical diffusion only for unstable stratification
- *Cloud species*
- *Moist Richardson number* (Brinkop, 1991; 1992)


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Short Description of the GCM ECHAM5 (8 of 8) Lecture 4: Numerical Formulation, page 82

**1.4 Physical parameterization**

- **Horizontal diffusion:** (Laursen and Eliassen, 1989)
- *Scale selective operator* applied beyond a threshold wave number
- **Gravity wave drag** (Palmer et al, 1986; Miller et al, 1989)
- *Surface stress due to gravity waves*, which are excited by stably stratified flow over irregular terrain is calculated from linear theory and dimensional considerations
- *Orographic forcing* prescribed as a directionally dependent sub-grid scale orographic variance computed from the high resolution USGS GTOPO30 data set
- *Vertical structure of momentum flux* induced by gravity waves calculated from a local wave Richardson number, which describes the onset of turbulence due to convective instability and the turbulent breakdown approaching a critical level
- *The GWD scheme* is not used at T21 resolution

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Lecture 4: Numerical Formulation, page 83

End of Lecture 4

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